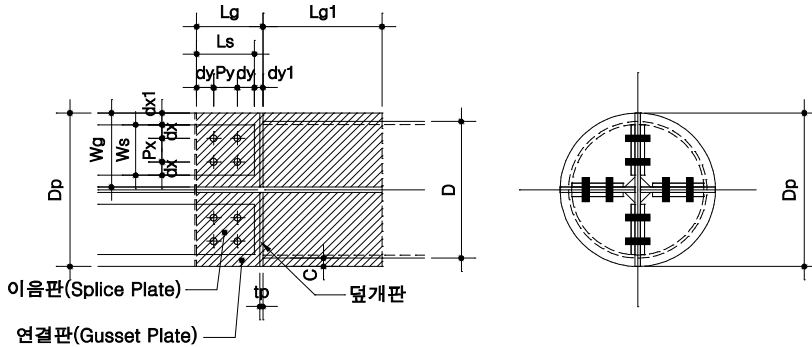


1. 설계조건

* 원형강관 $F_y = 235 \text{ MPa}$ $D = \phi 406.4 \text{ mm}$ $A_g = 11200 \text{ mm}^2$
 $F_u = 400 \text{ MPa}$ $t = 9 \text{ mm}$

* 덮개판
 $F_{ye} = 235 \text{ MPa}$ $D_p = \phi 456.4 \text{ mm}$
 $F_{ue} = 400 \text{ MPa}$ $t_p = 9 \text{ mm}$
 $C = (D_p - D) / 2 = (456.4 - 406.4) / 2 = 25.0 \text{ mm}$



2. 소요인장응력

$$\phi P_n = \phi t * F_y * A_g = 0.9 * 235 * 11200 * 1/10^3 = 2368.8 \text{ kN}$$

$$\phi P_n = \phi t * F_u * A_e = \phi t * F_u * U * A_n = 0.75 * 400 * 0.899 * 10552 * 1/10^3 = 2845.9 \text{ kN}$$

$$A_n = A_g - 4 * (t_g + 2) * t = 11200 - 4 * (16 + 2) * 9 = 10552 \text{ mm}^2$$

$$U = 1 - x / L_{g1} = 1 - 35.22 / 350 = 0.899$$

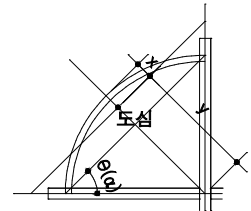
$$R = D / 2 = 406.4 / 2 = 203.2 \text{ mm} \quad r = (D - 2 * t) / 2 = (406.4 - 2 * 9) / 2 = 194.2 \text{ mm}$$

$$\theta = 45^\circ \quad \alpha = \theta * \pi / 180 = 45 * \pi / 180 = 0.7854 \text{ rad}$$

$$y = (2/3) * (R^3 - r^3) / (R^2 - r^2) * 180 / (\theta * \pi) * \sin \alpha$$

$$= (2/3) * (203.2^3 - 194.2^3) / (203.2^2 - 194.2^2) * 180 / (45 * \pi) * \sin(0.7854) = 178.9 \text{ mm}$$

$$x = y - R * \sin \alpha = 178.9 - 203.2 * \sin(0.7854) = 35.22 \text{ mm}$$



$\therefore P_{u, req} = \text{MIN}(2368.8, 2845.9) = 2368.8 \text{ kN}$
 $P_u = P_{u, req} / 4 = 2368.8 / 4 = 592.2 \text{ kN}$

3. 십자리브연결판 및 이음판 검토

1) 고력볼트 / 마찰접합 검토

(1group당)

고력볼트	직경 Db(mm)	구멍직경 Dbh(mm)	열수 Nx(열)	행수 Ny(행)	전체개수 N(EA)	볼트간격 Px(mm)	볼트간격 Py(mm)	연단거리 dx(mm) dx1(mm)	연단거리 dy(mm) dy1(mm)
F10T	M20	22	2	2	4	70	70	40 35.2	50 25

$W_{g, req} \geq (N_x - 1) * P_x + 2 * dx + dx1 = (2 - 1) * 70 + 2 * 40 + 35.2 = 185.2 \text{ mm}$
 $L_{g, req} \geq (N_y - 1) * P_y + 2 * dy + dy1 = (2 - 1) * 70 + 2 * 50 + 25 = 195.0 \text{ mm}$

$\phi = 1.00$ $\mu = 0.50$ (블라스트 후 페인트하지 않은 경우)
 $h_f = 1.00$ $F_u = 1000 \text{ MPa}$ $A_b = 314.2 \text{ mm}^2 / \text{EA}$ 전단면의 수 $N_s = 2$

설계볼트장력

$T_o = 0.70 * F_u * 0.75 * A_b = 0.70 * 1000 * 0.75 * 314.2 = 165.0 \text{ kN/EA}$

$\phi R_n = \phi * \mu * h_f * T_o * N_s = 1 * 0.5 * 1 * 165 * 2 = 165.0 \text{ kN/EA}$

$\therefore P_{u, req} / \phi R_n = 2368.8 / 165 = 14.36 \text{ EA} \leq 16 \text{ EA} \dots \text{OK}$

2) 이음판(Splice Plate)

(1group당)

Fys = 235 MPa
Fus = 400 MPa

매수	폭	길이	두께	면적	구멍개수	구멍직경	공제면적
	Ws (mm)	Ls (mm)	ts (mm)	(mm ²)		(mm)	(mm ²)
2	150	170	12	3600	2	22	-1056
Σ			24	3600			-1056

(1) 인장항복강도

Ag = 3600 mm²
 $\phi Pn = \phi t * Fys * Ag = 0.9 * 235 * 3600 * 1/10^3 * 4group = 3045.6 \text{ kN}$
 $\therefore Pu, req / \phi Pn = 2368.8 / 3045.6 = 0.78 \leq 1.00 \dots OK$

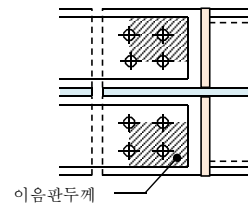
(2) 인장파단강도

U = 1.00
 An = MIN(3600 + (-1056), 0.85*Ag) = MIN(2544, 0.85*3600) = 2544.0 mm²
 $\phi Pn = \phi t * Fus * Ae = \phi t * Fus * U * An = 0.75 * 400 * 1 * 2544 * 1/10^3 * 4group = 3052.8 \text{ kN}$
 $\therefore Pu, req / \phi Pn = 2368.8 / 3052.8 = 0.78 \leq 1.00 \dots OK$

(3) 블록전단강도

L = (Ny-1)*Py = (2-1)*70 = 70.0 mm
 * 인장저항 순단면적
 Ant = Agt - Dbh*(Nx-0.5)*ts = 2640-22*(2-0.5)*24 = 1848.0 mm²
 * 인장저항 총단면적
 Agt = (Px + dx)*ts = (70 + 40)*24 = 2640.0 mm²
 * 전단저항 순단면적
 Anv = Agv - Dbh*(Ny-0.5)*ts = 2880 - 22*(2-0.5)*24 = 2088.0 mm²
 * 전단저항 총단면적
 Agv = (L + dy)*ts = (70 + 50)*24 = 2880.0 mm²

Fus*Ant = 400*1848 *1/10³ = 739.2 kN
 0.6*Fus*Anv = 0.6*400*2088 *1/10³ = 501.1 kN
 Fys*Agt = 235*2640 *1/10³ = 620.4 kN
 0.6*Fys*Agv = 0.6*235*2880 *1/10³ = 406.1 kN



Ubs = 1.00
 $\phi Pn = \phi t * (Ubs * Fus * Ant + \text{MIN}(0.6 * Fus * Anv, 0.6 * Fys * Agv))$
 $= 0.75 * (1 * 739.2 + \text{MIN}(501.1, 406.1)) * 4group = 3435.9 \text{ kN}$
 $\therefore Pu, req / \phi Pn = 2368.8 / 3435.9 = 0.69 \leq 1.00 \dots OK$

3) 심자리브연결판(Gusset Plate)

(1group당)

Fyg = 235 MPa
Fug = 400 MPa
Lg1 = 350 mm

매수	폭	길이	두께	면적	구멍개수	구멍직경	공제면적
	Wg (mm)	Lg (mm)	tg (mm)	(mm ²)		(mm)	(mm ²)
1	220.2	195	16	3523.2	2	22	-704
Σ			16	3523.2			-704

폭두께비 b/t = Wg/Tg = 220.2/16 = 13.76 < 15.00 ...OK

(1) 인장항복강도

Ag = 3523.2*4group + 16*16(교차부) = 14348.8 mm²
 $\phi Pn = \phi t * Fyg * Ag = 0.9 * 235 * 14348.8 * 1/10^3 = 3034.8 \text{ kN}$
 $\therefore Pu, req / \phi Pn = 2368.8 / 3034.8 = 0.78 \leq 1.00 \dots OK$

(2) 인장파단강도

U = 1.00
 An = MIN(14348.8 + (-704*4group), 0.85*Ag) = MIN(11532.8, 0.85*14348.8) = 11532.8 mm²
 $\phi Pn = \phi t * Fug * Ae = \phi t * Fug * U * An = 0.75 * 400 * 1 * 11532.8 * 1/10^3 = 3459.8 \text{ kN}$
 $\therefore Pu, req / \phi Pn = 2368.8 / 3459.8 = 0.68 \leq 1.00 \dots OK$

(3) 블록전단강도

$$L = (N_y - 1) \cdot P_y = (2 - 1) \cdot 70 = 70.0 \text{ mm}$$

* 인장저항 순단면적

$$A_{nt} = A_{gt} - D_{bh} \cdot (N_x - 0.5) \cdot t_g = 2323.2 - 22 \cdot (2 - 0.5) \cdot 16 = 1795.2 \text{ mm}^2$$

* 인장저항 총단면적

$$A_{gt} = (P_x + d_x + d_{x1}) \cdot t_g = (70 + 40 + 35.2) \cdot 16 = 2323.2 \text{ mm}^2$$

* 전단저항 순단면적

$$A_{nv} = A_{gv} - D_{bh} \cdot (N_y - 0.5) \cdot t_g = 1920 - 22 \cdot (2 - 0.5) \cdot 16 = 1392.0 \text{ mm}^2$$

* 전단저항 총단면적

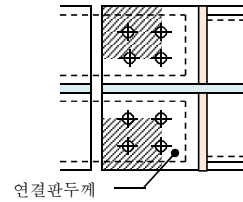
$$A_{gv} = (L + d_y) \cdot t_g = (70 + 50) \cdot 16 = 1920.0 \text{ mm}^2$$

$$F_{ug} \cdot A_{nt} = 400 \cdot 1795.2 \cdot 1/10^3 = 718.1 \text{ kN}$$

$$0.6 \cdot F_{ug} \cdot A_{nv} = 0.6 \cdot 400 \cdot 1392 \cdot 1/10^3 = 334.1 \text{ kN}$$

$$F_{yg} \cdot A_{gt} = 235 \cdot 2323.2 \cdot 1/10^3 = 546.0 \text{ kN}$$

$$0.6 \cdot F_{yg} \cdot A_{gv} = 0.6 \cdot 235 \cdot 1920 \cdot 1/10^3 = 270.7 \text{ kN}$$



$$U_{bs} = 1.00$$

$$\phi P_n = \phi t \cdot (U_{bs} \cdot F_{ug} \cdot A_{nt} + \text{MIN}(0.6 \cdot F_{ug} \cdot A_{nv}, 0.6 \cdot F_{yg} \cdot A_{gv}))$$

$$= 0.75 \cdot (1 \cdot 718.1 + \text{MIN}(334.1, 270.7)) \cdot 4_{group} = 2966.4 \text{ kN}$$

$$\therefore P_u, req / \phi P_n = 2368.8 / 2966.4 = 0.80 \leq 1.00 \dots \text{OK}$$

4) 심자리브연결판 교차부 용접부 / 1group당

용접재 인장강도 $F_{uw1} = 420 \text{ MPa}$

- 용접치수

$$S_{w1} = 7.00 \text{ mm} \quad n_{w1} = 2 \text{ 개소/1group당} \quad \text{필릿용접(1)/완전용입용접(2)} : 1$$

$$L_{we1} = L_g + L_{g1} - 2 \cdot S_{w1} = 195 + 350 - 2 \cdot 7 = 531.0 \text{ mm}$$

$$A_{w1} = n_{w1} \cdot (0.707 \cdot S_{w1}) \cdot L_{we1} = 2 \cdot (0.707 \cdot 7) \cdot 531 = 5255.8 \text{ mm}^2$$

$$\phi R_{nw} = \phi \cdot F_w \cdot A_{w1} = \phi \cdot 0.6 \cdot F_{uw1} \cdot A_{w1} = 0.75 \cdot 0.6 \cdot 420 \cdot 5255.8 \cdot 1/10^3 = 993.3 \text{ kN}$$

$$\therefore P_u / \phi R_{nw} = 592.2 / 993.3 = 0.60 \leq 1.00 \dots \text{OK}$$

$$\phi R_n = \phi \cdot 0.6 \cdot F_{ug} \cdot t_g \cdot L_{we1} = 0.75 \cdot 0.6 \cdot 400 \cdot 16 \cdot 531 \cdot 1/10^3 = 1529.3 \text{ kN}$$

$$\therefore P_u / \phi R_n = 592.2 / 1529.3 = 0.39 \leq 1.00 \dots \text{OK}$$

$$\phi R_n = \phi \cdot 0.6 \cdot F_{yg} \cdot t_g \cdot L_{we1} = 1 \cdot 0.6 \cdot 235 \cdot 16 \cdot 531 \cdot 1/10^3 = 1197.9 \text{ kN}$$

$$\therefore P_u / \phi R_n = 592.2 / 1197.9 = 0.49 \leq 1.00 \dots \text{OK}$$

5) 심자리브연결판 원형강관 용접부 / 1group당

용접재 인장강도 $F_{uw2} = 420 \text{ MPa}$

- 용접치수

$$S_{w2} = 7.00 \text{ mm} \quad n_{w2} = 2 \text{ 개소/1group당} \quad \text{필릿용접(1)/완전용입용접(2)} : 1$$

$$L_{we2} = L_{g1} - 2 \cdot S_{w2} = 350 - 2 \cdot 7 = 336.0 \text{ mm}$$

$$A_{w2} = n_{w2} \cdot (0.707 \cdot S_{w2}) \cdot L_{we2} = 2 \cdot (0.707 \cdot 7) \cdot 336 = 3325.7 \text{ mm}^2$$

$$\phi R_{nw} = \phi \cdot F_w \cdot A_{w2} = \phi \cdot 0.6 \cdot F_{uw2} \cdot A_{w2} = 0.75 \cdot 0.6 \cdot 420 \cdot 3325.7 \cdot 1/10^3 = 628.6 \text{ kN}$$

$$\therefore P_u / \phi R_{nw} = 592.2 / 628.6 = 0.94 \leq 1.00 \dots \text{OK}$$

$$F_{ug} \cdot t_g = 6400 \text{ N/mm} \leq F_u \cdot t \cdot 2 = 7200 \text{ N/mm}$$

$$\phi R_n = \phi \cdot 0.6 \cdot F_{ug} \cdot t_g \cdot L_{we2} = 0.75 \cdot 0.6 \cdot 6400 \cdot 336 \cdot 1/10^3 = 967.7 \text{ kN}$$

$$\therefore P_u / \phi R_n = 592.2 / 967.7 = 0.61 \leq 1.00 \dots \text{OK}$$

$$F_{yg} \cdot t_g = 3760 \text{ N/mm} \leq F_y \cdot t \cdot 2 = 4230 \text{ N/mm}$$

$$\phi R_n = \phi \cdot 0.6 \cdot F_{yg} \cdot t_g \cdot L_{we2} = 1 \cdot 0.6 \cdot 3760 \cdot 336 \cdot 1/10^3 = 758.0 \text{ kN}$$

$$\therefore P_u / \phi R_n = 592.2 / 758 = 0.78 \leq 1.00 \dots \text{OK}$$

* 필릿용접인 경우 여장

$$C, req = \text{MAX}(25, S_{w2} + t_{g, req}) = \text{MAX}(25, 7 + 16) = 25.0 \text{ mm} \leq C = 25 \text{ mm} \dots \text{OK}$$

4. 덮개판과 원형강관 용접부 검토

- 용접치수

Sw3 = 7.00 mm (필릿용접)

- 덮개판에는 특별히 작용하는 하중은 없으나, 연결판의 좌굴방지 및 강관 내부 부식방지를 위하여 필릿용접한다.